

## Tribology and *ex vivo* analysis: hip and knee prostheses

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23 September 2013

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## A clinical and engineering collaboration

Title / Author	Cited by	Year
Early failure of metal-on-metal bearings in hip resurfacing and large diameter total hip replacement: A CONSEQUENCE OF EXCESS WEAR DJ Langton, SS Jameson, TJ Joyce, J Webb, AVF Nargol <i>Journal of Bone &amp; Joint Surgery, British Volume</i> 92 (1), 38-46	234	2010
The effect of component size and orientation on the concentrations of metal ions after resurfacing arthroplasty of the hip DJ Langton, SS Jameson, TJ Joyce, J Webb, AVF Nargol <i>Journal of Bone &amp; Joint Surgery, British Volume</i> 92 (9), 1143-1151	166	2008
Blood metal ion concentrations after hip resurfacing arthroplasty A COMPARATIVE STUDY OF ARTICULAR SURFACE REPLACEMENT AND BIRMINGHAM HIP RESURFACING ARTHROPLASTIES DJ Langton, JP Sprowson, TJ Joyce, M Reed, J Carluke, P Partington, AVF Nargol <i>Journal of Bone &amp; Joint Surgery, British Volume</i> 91 (10), 1287-1295	106	2009
Adverse reaction to metal debris following hip resurfacing the influence of component type, orientation and volumetric wear DJ Langton, TJ Joyce, SS Jameson, J Lord, M Van Oosswij, JP Holland, AVF Nargol <i>Journal of Bone &amp; Joint Surgery, British Volume</i> 93 (2), 164-171	90	2011
Accelerating failure rate of the ASR total hip replacement DJ Langton, SS Jameson, TJ Joyce, JN Gandhi, R Sidagimamale, P Mereddy, J ... <i>Journal of Bone &amp; Joint Surgery, British Volume</i> 93 (8), 1011-1016	87	2011



## Overview

- Tribology
- Why undertake *ex vivo* analysis
- Hip prostheses
- Knee prostheses



## TRIBOLOGY



## Tribology fundamentals

Jin et al, *Biotribology*, *Current Orthopaedics*, 2006, 20, 1, 32-40

Joyce, *Biopolymer Tribology*, in *Polymer Tribology*, Imperial College Press, 2009, 227-266

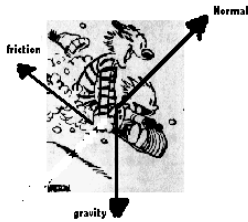


## Definition of tribology

- Tribology, from the Greek *tribos* 'to rub'
- The science of interacting surfaces in relative motion, including friction, lubrication and wear
- Biotribology is this science related to the body
- Primarily synovial joints and replacement joints



## Friction



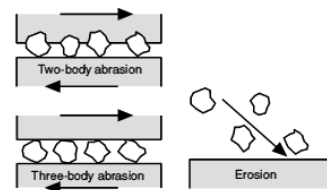
## Friction (1)

- Friction force is a resistance to motion
- With no lubricant:
  - Friction force is proportional to normal force  $F = \mu N$
  - Friction is independent of velocity
  - Friction is independent of apparent contact area
  - Friction is dependent on real contact area (1 to 0.0001% of apparent contact area)

## Friction (2)

- Friction force ( $F$ ) =  $F_{\text{adhesion}} + F_{\text{ploughing}}$ 
  - Due to chemical bonding at the asperity contacts
  - Due to breaking and deforming of one asperity by another

## Wear




## Wear (1)

- Wear is the progressive loss of material from a surface. Various wear regimes:
    - Adhesive – due to bonding
    - Abrasive – due to hard asperities
    - Fatigue – due to cyclic stresses
    - Erosive – due to relative motion with a fluid containing hard particles
    - Corrosive – due to chemical reactions
- May occur singly or in combination*



## Wear (2)

- Wear can be measured as a depth, but volume is much better
- Generally wear volumes:
  - Increase with load
  - Increase with sliding distance
  - Increase with surface roughness
  - Decrease with surface hardness
- However, many other factors can be involved in the wear process

# Lubrication

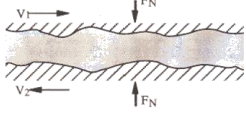


Adds a fluid film to separate surfaces

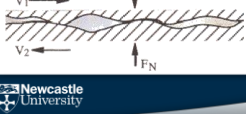



## Lubrication regimes



**Hydrodynamic regime**



**Boundary lubrication**





- Indicated by lambda ratio,  $\lambda$
- Hydrodynamic lubrication ( $\lambda > 3$ )
- Mixed lubrication ( $1 < \lambda < 3$ )
- Boundary lubrication ( $\lambda < 1$ )
- Metal-on-polyethylene implants operate under boundary lubrication

## Calculation of lubrication regimes



$$\lambda = \frac{h_{min}}{\left[ (R_{a1})^2 + (R_{a2})^2 \right]^{1/2}} \quad \frac{h_{min}}{R_x} = 2.80 \left( \frac{\eta u}{E^* R_x} \right)^{0.65} \left( \frac{w}{E^* R_x^2} \right)^{-0.21}$$

- $R_{a1}$  and  $R_{a2}$  are the surface roughness values of each component,  $h_{min}$  is the minimum effective film thickness,  $R_x$  is the equivalent radius (m),  $\eta$  is the viscosity of the lubricant (Pa s),  $u$  is the entraining velocity (m/s),  $E^*$  is the equivalent elastic modulus (Pa), and  $w$  is the load (N)

$$\frac{1}{R_x} = \frac{1}{R_1} - \frac{1}{R_2} \quad \frac{1}{E^*} = 0.5 \left( \frac{1 - \nu_1^2}{E_1} + \frac{1 - \nu_2^2}{E_2} \right)$$





## Calculation of lubrication regimes

Implant type	Dia. (mm)	Roughness, head and cup (nm Ra)	Lubrication regime ( $\lambda$ value)
Metal-on-polymer total hip replacement	28		
Metal-on-metal total hip replacement	28		
Metal-on-metal hip resurfacing	52		



## Calculation of lubrication regimes

Implant type	Dia. (mm)	Roughness, head and cup (nm Ra)	Lubrication regime ( $\lambda$ value)
Metal-on-polymer total hip replacement	28	20, 1500	
Metal-on-metal total hip replacement	28	20, 20	
Metal-on-metal hip resurfacing	52	20, 20	

## Calculation of lubrication regimes

Implant type	Dia. (mm)	Roughness, head and cup (nm Ra)	Lubrication regime ( $\lambda$ value)
Metal-on-polymer total hip replacement	28	20, 1500	Boundary lubrication ( $\lambda < 1$ )
Metal-on-metal total hip replacement	28	20, 20	Mixed lubrication ( $1 < \lambda < 3$ )
Metal-on-metal hip resurfacing	52	20, 20	Fluid film lubrication ( $\lambda > 3$ )

## Different Hip Resurfacing Designs



Implant	Revision rate at 5 years
ASR	13.8%

Source: National Joint Registry for England and Wales 2012

## Different Hip Resurfacing Designs



Implant	Revision rate at 5 years
ASR	13.8%
BHR	3.7%

Source: National Joint Registry for England and Wales 2012

## Different Hip Resurfacing Designs



Implant	Revision rate at 5 years
ASR	13.8%
BHR	3.7%
Conserve +	8.5%

Source: National Joint Registry for England and Wales 2012

## Different Hip Resurfacing Designs



Implant	Revision rate at 5 years
ASR	13.8%
BHR	3.7%
Conserve +	8.5%
Durom	6.0%

Source: National Joint Registry for England and Wales 2012

## Why *ex vivo* analysis?

- To learn from failures to prevent future failures
- Patients get better implants
- Costs reduced due to fewer revision operations
- Failure could be due to:
  - Design defect
  - Poor surgical instruments/training
- Ensure the orthopaedic surgeon doesn't mistakenly get blamed

## HIPS

## The Lancet 2007



**The operation of the century: total hip replacement**  
Jan O. Lemanmonth, Claire Young, Cedric Barabec

Issue 3601, 3704-3708-13  
 Published Online  
 March 26, 2007  
 DOI:10.1016/S0140-6736(07)60467-2  
 0140-6736(07)60467-2

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In the 1960s, total hip replacement revolutionised management of elderly patients crippled with arthritis, with very good long-term results. Today, young patients present for hip-replacement surgery hoping to restore their quality of life, which typically includes physically demanding activities. Advances in bioengineering technology have driven development of hip prostheses. Both cemented and cementless hips can provide durable fixation. Better materials and design have allowed use of large-bore bearings, which provide an increased range of motion with enhanced stability and very low wear. Minimally invasive surgery limits soft-tissue damage and facilitates accelerated discharge and rehabilitation. Short-term objectives must not compromise long-term performance. Computer-assisted surgery will contribute to reproducible and accurate placement of implants. Universal economic constraints in healthcare services dictate that further developments in total hip replacement will be governed by their cost-effectiveness.

- 'Charnley LFA: a worldwide retrospective review at 15 to 20 years' (Older, J Arthroplasty, 2002, 675-680). 83% survival rate at 20 years
- National Joint Registry (NJR) 2012 – 97.7% survival rate at 8 years (cemented hips)



**Mail on Sunday**  
**24 Oct 2010**  
**DePuy ASR™**  


## November 2011

- Australian Senate report
- "The committee is deeply disturbed by what appears to be tardiness on the part of JJM to act on known problems with these devices. Many people could have avoided considerable pain, suffering and diminished quality of life if the company had acted in a responsible manner"



The Senate

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Community Affairs  
References Committee

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The regulatory standards for the approval of  
medical devices in Australia

## May/Nov 2012



- UK Government
- "When things go wrong with implants it can ruin lives— as the complications with metal-on-metal hip replacements have sadly shown"
- "Much greater transparency is needed about the approval process"



## 2013

**The Telegraph**

### Jury orders J&J unit to pay \$8.3 million in metal hip trial

By Deena Beasley  
 Fri Mar 8, 2013 3:31pm EST

(Reuters) - A Los Angeles jury ordered Johnson & Johnson's DePuy orthopaedic unit to pay more than **\$8 million** in damages in the first trial of nearly **11,000 lawsuits** filed over the company's recalled artificial metal hips.

In a mixed verdict, the Los Angeles Superior Court jury on Friday found that the hips were defective, but that DePuy did not act with fraud or malice. DePuy was ordered to pay more than \$338,000 in medical costs and \$8 million for pain and suffering to plaintiff Loren Kransky. No punitive damages were awarded.





## Monitoring the Introduction and Performance of a Joint Replacement: The United Kingdom Metal-on-Metal Alert

JBJS (US) 2011

Keith Tucker, FRCS, Paul Gregg, MD, FRCS, Peter Kay, FRCS, Martyn Porter, FRCS,  
 Peter Howard, FRCS, Martin Pickford, PhD, and Crina Cacosu, PhD  
*Investigation performed at the National Joint Registry of England and Wales*

- "Data critical of the performance of the ASR were presented at numerous scientific meetings in 2008 and onward to the time of this writing, particularly at meetings of the British Hip Society (BHS) and the British Orthopaedic Association (BOA). This factor, rather than the MHRA alert in July 2010, almost certainly led to the subsequent drop in sales of that implant"

## Who criticised ASR in 2008?

- **Hip resurfacing in females – are we under-diagnosing metal hypersensitivity?** DJ Langton, SS Jameson, T Joyce, J Webb, AVF Nargol. British Hip Society, Norwich, February 2008
- **Analysis of ex vivo resurfacing hip prostheses and comparison with clinical data.** T Joyce, D Langton, S Jameson, AVF Nargol. British Orthopaedic Research Society, Manchester, June 2008
- **Analysis of failed metal-on-metal resurfacing hip prostheses.** TJ Joyce, DJ Langton, SS Jameson, AVF Nargol. Bath Biomechanics Symposium, Bath, 15 September 2008
- **Reducing exposure to metal ions following hip resurfacing: the importance of acetabular orientation.** DJ Langton, SS Jameson, TJ Joyce, J Webb and A V F Nargol. British Orthopaedic Association 2008 annual congress, Liverpool, September 2008
- **Early aseptic failure of large metal-on-metal hip arthroplasty – is metal sensitivity a consequence of excess wear?** DJ Langton, SS Jameson, TJ Joyce, J Webb, AVF Nargol. British Orthopaedic Association 2008 annual congress, Liverpool, September 2008



## The effect of component size and orientation on the concentrations of metal ions after resurfacing arthroplasty of the hip

JBJS (UK) Sept 2008, 1143-1151

D. J. Langton,  
S. S. Jameson,  
T. J. Joyce,  
J. Webb,  
A. V. F. Nargol

From the University  
Hospital of North  
Tees, Stockton-on-  
Tees, England

Increased concentrations of metal ions after metal-on-metal resurfacing arthroplasty of the hip remain a concern. Although there has been no proven link to long-term health problems or early prosthetic failure, variables associated with high metal ion concentrations should be identified and, if possible, corrected. Our study provides data on metal ion levels from a series of 76 consecutive patients (76 hips) after resurfacing arthroplasty with the Articular Surface Replacement. Chromium and cobalt ion concentrations in the whole blood of patients with smaller (< 51 mm) femoral components were significantly higher than in those with the larger (> 53 mm) components ( $p < 0.01$ ). Ion concentrations in the former group were significantly related to the inclination ( $p = 0.01$ ) and anteversion ( $p = 0.01$ ) of the acetabular component. The same relationships were not significant in the patients with larger femoral components ( $p = 0.61$  and  $p = 0.49$ , respectively). Accurate positioning of the acetabular component intra-operatively is essential in order to reduce the concentration of metal ions in the blood after hip resurfacing arthroplasty with the Articular Surface Replacement implant.

For DePuy ASR™ hip resurfacings ion levels linked to acetabular cup size and position



## Blood metal ion concentrations after hip resurfacing arthroplasty

A COMPARATIVE STUDY OF ARTICULAR SURFACE REPLACEMENT AND BIRMINGHAM HIP RESURFACING ARTHROPLASTIES

JBJS (UK) Oct 2009

D. J. Langton,  
A. P. Sprowson,  
T. J. Joyce,  
M. Reed,  
I. Calalce,  
P. Farrington,  
A. V. F. Nargol

From University  
Hospital of North  
Tees and Newcastle  
University, Newcastle  
upon Tyne, England

There have been no large comparative studies of the blood levels of metal ions after implantation of commercially available hip resurfacing devices which have taken into account the effects of femoral size and inclination and anteversion of the acetabular component. We present the results in 90 patients with unilateral articular surface replacement (ASR) hip resurfacings (mean time to blood sampling 26 months) and 76 patients with unilateral Birmingham Hip Resurfacing (BHR) implants (mean time 47 months).

The whole blood and serum chromium (Cr) and cobalt (Co) concentrations were inversely related to the size of the femoral component. In both groups ( $p < 0.05$ ), Cr and Co were more strongly influenced by the position of the acetabular component in the case of the ASR, with an increase in metal ions observed at inclinations  $> 45^\circ$  and anteversion angles of  $< 10^\circ$  and  $> 20^\circ$ . These levels were only increased in the BHR group when the acetabular component was implanted with an inclination  $< 55^\circ$ .

A significant relationship was identified between the anteversion of the BHR acetabular component and the levels of Cr and Co ( $p < 0.05$  for Co), with an increase observed at anteversion angles  $< 10^\circ$  and  $> 20^\circ$ . The median whole blood and serum Cr concentrations of the male ASR patients were significantly lower than those of the BHR men ( $p < 0.001$ ). This indicates that reduced diametral clearance may equate to a reduction in metal ion concentrations in larger joints with satisfactory orientation of the acetabular component.

Contact Patch to Rim (CPR) distance – ASR™ cups more sensitive to position than BHR: explains differences in clinical results



## Early failure of metal-on-metal bearings in hip resurfacing and large-diameter total hip replacement

A CONSEQUENCE OF EXCESS WEAR

JBJS (UK) Jan 2010

D. J. Langton,  
S. S. Jameson,  
T. J. Joyce,  
N. J. Hallab,  
S. Natsu,  
A. V. F. Nargol

From North Tees and  
Hartlepool NHS  
Trust, Stockton-on-  
Tees and Centre for  
Rehabilitation,  
Newcastle University,  
Newcastle upon

Early failure associated with adverse reactions to metal debris is an emerging problem after hip resurfacing but the exact mechanism is unclear. We analysed our entire series of 660 metal-on-metal resurfacings (Articular Surface Replacement (ASR) and Birmingham Hip Resurfacing (BHR)) and large-bearing ASR total hip replacements, to establish associations with metal debris-related failures. Clinical and radiological outcomes, metal ion levels, explant studies and lymphocyte transformation tests were performed. A total of 17 patients (3.4%) were identified (all ASR bearings) with adverse reactions to metal debris, for which revision was required. This group had significantly smaller components, significantly higher acetabular component anteversion, and significantly higher whole concentrations of blood and joint chromium and cobalt ions than asymptomatic patients did (all  $p < 0.001$ ). Post-revision lymphocyte transformation tests on this group showed no reactivity to chromium or cobalt ions. Explants from these revisions had greater surface wear than retrievals for uncomplicated fractures. The absence of adverse reactions to metal debris in patients with well-positioned implants usually implies high component wear.



## Accelerating failure rate of the ASR total hip replacement

JBJS (UK) Aug 2011

D. J. Langton,  
S. S. Jameson,  
T. J. Joyce,  
J. N. Gandhi,  
R. Sidaginamale,  
P. Meredith,  
J. Lord,  
A. V. F. Nargol

From the University  
Hospital of North  
Tees, Stockton,  
United Kingdom

There is widespread concern regarding the incidence of adverse soft-tissue reactions after metal-on-metal (MoM) hip replacement. Recent National Joint Registry data have shown clear differences in the rates of failure of different designs of hip resurfacing. Our aim was to update the failure rates related to metal debris for the Articular Surface Replacement (ASR). A total of 506 of these were implanted.

Kaplan-Meier analysis showed a failure rate of 25% at six years for the ASR resurfacing and of 48.8% for the ASR total hip replacement (THR). Of 257 patients with a minimum follow-up of two years, 67 (26.1%) had a serum cobalt concentration which was greater than 7 µg/l. Co-ordinate measuring machine analysis of revised components showed that all patients suffering adverse tissue reactions in the resurfacing group had abnormal wear of the bearing surfaces. Six THR patients had relatively low rates of articular wear, but were found to have considerable damage at the trunion-taper interface. Our results suggest that wear at the modular junction is an important factor in the development of adverse tissue reactions after implantation of a large-diameter MoM THR.

ASR XL 49% revision rate at 6 yrs  
Identification of damage at taper interface



## Taper junction failure in large-diameter metal-on-metal bearings

D. J. Langton,  
R. Sidaginamale,  
J. K. Lord,  
A. V. F. Nargol,  
T. J. Joyce

From Newcastle  
University, Newcastle  
upon Tyne, United  
Kingdom

**Objectives**  
An ongoing prospective study to investigate failing metal-on-metal hip prostheses was commenced at our centre in 2008. We report on the results of the analysis of the first consecutive 126 failed mated total hip prostheses from a single manufacturer.

**Methods**  
Analysis was carried out using highly accurate coordinate measuring to calculate volumetric and linear rates of the articular bearing surfaces and also the surfaces of the taper junctions. The relationship between taper wear rates and a number of variables, including bearing diameter and orientation of the acetabular component, was investigated.

- Bone & Joint Research, 2012, 1, 4, 56-63
- Measurement of taper wear volumes



SPECIAL ISSUE PAPER 317

### Tribological analysis of failed resurfacing hip prostheses and comparison with clinical data

T J Joyce<sup>a</sup>, D J Langton<sup>a</sup>, S S Jameson<sup>a</sup>, and A V F Nargol<sup>b</sup>  
<sup>a</sup>Centre for Rehabilitation and Engineering Studies, School of Mechanical and Systems Engineering, Newcastle University, Newcastle upon Tyne, UK  
<sup>b</sup>Joint Replacement Unit, University Hospital of North Tees, Hardwick, Stockton-on-Tees, UK

The manuscript was received on 21 July 2008 and was accepted after revision for publication on 8 January 2009.  
 DOI: 10.1243/13506501JET484

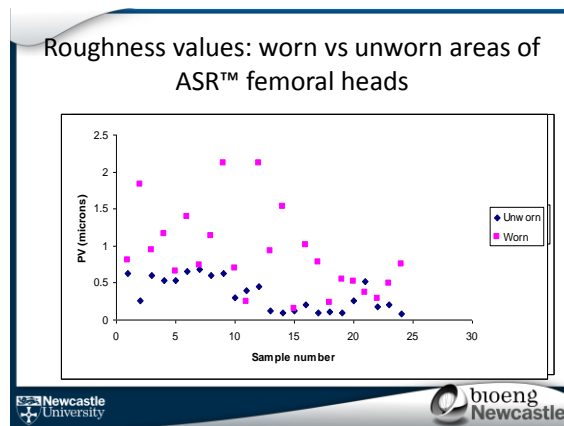
J Engineering Tribology, 2009, 317-323

#### Failed ASR™ resurfacing hips had roughened in the body

**Abstract:** Metal-on-metal resurfacing hip prostheses offer potential benefits over total hip replacement for younger and more active patients. Although some reported clinical results of resurfacing hip prostheses are excellent, other outcomes are less positive. To aid with understanding the balance of benefits related to these devices, analysis of failed resurfacing prostheses can contribute critical insights. However, because these implants are so new there are relatively few such prostheses available for independent *ex vivo* analysis. From a single-surgeon clinical cohort, a number of failed resurfacing hip prostheses were obtained and studied. It was found that roughness values of the articulating surfaces had increased so that the theoretical lubrication regime would shift from the fluid film to the boundary. In turn, this would likely result in increased wear from the articulating surfaces. High ion levels were seen in the patients from whom the explants were obtained, thus supporting the hypothesis that wear was linked with failure of the explanted hip resurfacing prostheses.

**Keywords:** metal-on-metal, cobalt chrome, hip resurfacing, hip prostheses, explant

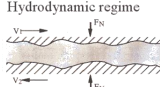
Newcastle University 



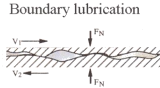
### Summary of roughness results

- Typical changes 15nm Ra to 60nm Ra
- Results in change from hydrodynamic to boundary lubrication
- In boundary lubrication, wear volume (V) is proportional to sliding distance (D)
- Hip resurfacings are large diameter, so wear could occur over a large sliding distance giving high wear volumes ....

Hydrodynamic regime




Boundary lubrication



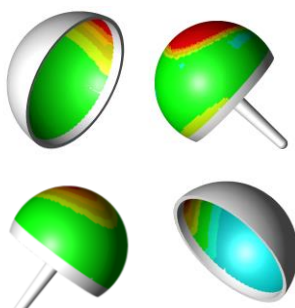
$$V = KFD$$

V = Volume lost (mm<sup>3</sup>)  
 K = Wear factor (x10<sup>-6</sup>mm<sup>3</sup>/Nm)  
 F = Load (N)  
 D = Sliding distance (m)


Newcastle University 



### Failed ASR™ resurfacings




Common factor – ‘rim wear’ at edge of cup. Associated with cups fitted at high inclination and/or anteversion angles

Newcastle University 

### Questions to you

- What is an acceptable wear rate *in vivo* for a metal-on-metal hip?
- How do you measure this wear *in vivo*?

Newcastle University 

Wear 272 (2011) 79–87

Contents lists available at ScienceDirect

Wear

journal homepage: [www.elsevier.com/locate/wear](http://www.elsevier.com/locate/wear)

Volumetric wear assessment of failed metal-on-metal hip resurfacing prostheses

J.K. Lord<sup>a,\*</sup>, D.J. Langton<sup>a</sup>, A.V.F. Nargol<sup>b</sup>, T.J. Joyce<sup>a</sup>

<sup>a</sup>School of Mechanical & Systems Engineering, Stephenson Building, Claremont Road, Newcastle University, Newcastle upon Tyne NE1 7RU, England, UK

<sup>b</sup>Joint Replacement Unit, University Hospital of North Tees, Hordwick Road, Stockton TS19 6PE, UK

- For ASR explants, average wear 18mm<sup>3</sup>/year
- 3mm<sup>3</sup>/year as ‘tipping point’ above which failure occurs

### Could *in vitro* wear testing of the ASR identified high wear?

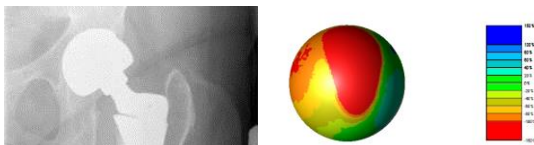
#### Tribology and Wear of Metal-on-Metal Hip Prostheses: Influence of Cup Angle and Head Position

Sophie Williams, Ian Leslie, Graham Isaac, Zhongmin Jin, Eileen Ingham and John Fisher

*J Bone Joint Surg Am.* 2008; 90:111-117. doi:10.2106/JBJS.H.00485

- Small resurfacing ASR tested at 55° inclination by Leeds University/DePuy
- 9mm<sup>3</sup>/million cycles wear (90x > large ASRs at 45°)
- Resurfacing patients do 1.9 million steps p.a.
- Average wear ASR resurfacing explants 18mm<sup>3</sup>/year (Lord *et al*, *Wear*, 2011)
- Hip simulators can provide clinically relevant results

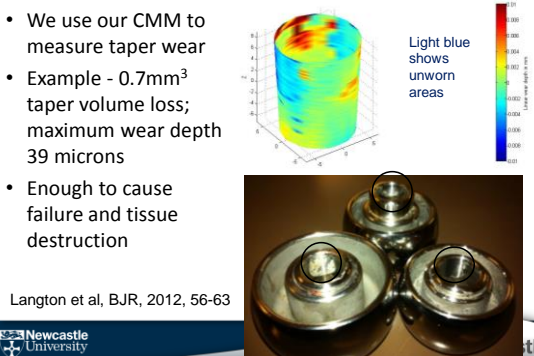
### ASR™ XL femoral head



- Female patient, ASR™, failure at 35 months
- 45.5mm diameter, inclination 60°, anteversion 31°: Co 32.2µg/L, Cr 22.0µg/L
- Red area shows at least 20µm of wear depth, wear volume from head 20.2mm<sup>3</sup>

### Wear at taper junction ASR™ XL

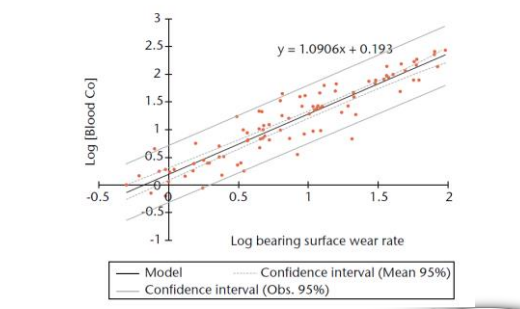
- We use our CMM to measure taper wear
- Example - 0.7mm<sup>3</sup> taper volume loss; maximum wear depth 39 microns
- Enough to cause failure and tissue destruction



Langton et al, *BJR*, 2012, 56-63

### A WORD ON IONS

### Plot wear rate v blood Co



Log [Blood Co]

Log bearing surface wear rate

$y = 1.0906x + 0.193$

— Model    — Confidence interval (Mean 95%)  
 — Confidence interval (Obs. 95%)

## The 'cobalt ladder'

Whole blood Cobalt	Interpretation
<1µg/l	93% of population

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4.5 to 5.6µg/l	High specificity for abnormal wear

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2 to 4.5µg/l	Abnormal wear possible. Consider device, bearing diameter, orientation in vivo and activity levels
4.5 to 5.6µg/l	High specificity for abnormal wear
>5.6µg/l	100% specific for abnormal wear

## The 'cobalt ladder'

Whole blood Cobalt	Interpretation
<1µg/l	93% of population
<2µg/l	Values are near to background. Expected wear of MoM resurfacings
2 to 4.5µg/l	Abnormal wear possible. Consider device, bearing diameter, orientation in vivo and activity levels
4.5 to 5.6µg/l	High specificity for abnormal wear
>5.6µg/l	100% specific for abnormal wear
>10µg/l	Abnormal wear unequivocal

## The 'cobalt ladder'

Whole blood Cobalt	Interpretation
<1µg/l	93% of population
<2µg/l	Values are near to background. Expected wear of MoM resurfacings
2 to 4.5µg/l	Abnormal wear possible. Consider device, bearing diameter, orientation in vivo and activity levels
4.5 to 5.6µg/l	High specificity for abnormal wear
>5.6µg/l	100% specific for abnormal wear
>10µg/l	Abnormal wear unequivocal
>20µg/l	Metal staining of the joint

## Bone Joint Research, 2013, 2, 84-95

BJR

HIP

### Blood metal ion testing is an effective screening tool to identify poorly performing metal-on-metal bearing surfaces

R. P. Sidaginamale,  
T. J. Joyce,  
J. K. Lord,  
R. Jefferson,  
P. G. Blain,  
A. V. F. Nargol,  
D. J. Langton

#### Objectives

The aims of this piece of work were to: 1) record the background concentrations of blood chromium (Cr) and cobalt (Co) concentrations in a large group of subjects; 2) to compare blood/serum Cr and Co concentrations with retrieved metal-on-metal (MoM) hip resurfacings; 3) to examine the distribution of Co and Cr in the serum and whole blood of patients with MoM hip arthroplasties; and 4) to further understand the partitioning of metal ions between the serum and whole blood fractions.

Open Access

Research



## The clinical implications of elevated blood metal ion concentrations in asymptomatic patients with MoM hip resurfacings: a cohort study

David J Langton, Raghavendra P Sidaginamale, Thomas J Joyce, Shonali Natu, Peter Blain, Robert Drysdale Jefferson, Stephen Rushton, Antoni V F Nargol

To cite: Langton DJ, Sidaginamale RP, Joyce TJ, et al. The clinical implications of elevated blood metal ion concentrations in asymptomatic patients with MoM hip resurfacings: a cohort study. *BMJ Open* 2013;3:e001541. doi:10.1136/bmjopen-2012-001541

**ABSTRACT**  
**Objective:** To determine whether elevated blood cobalt (Co) concentrations are associated with early failure of metal-on-metal (MoM) hip resurfacings secondary to adverse reaction to metal debris (ARMD).  
**Design:** Cohort study.  
**Setting:** Single centre orthopaedic unit.  
**Participants:** Following the identification of complications potentially related to metal wear debris, a cohort of metal ion concentration measurements was identified.

#### ARTICLE SUMMARY

**Article focus**  
• Current Food and Drug Administration guidance for the management of patients with MoM hips states that the utility of routine screening of asymptomatic patients using blood metal ion testing has not been established.  
• This study sought to document the clinical progress of asymptomatic patients with elevated

## KNEES

## Background



- Knee replacements are the most common joint replacement procedure in the UK and the world
- The number of operations increases every year and cannot solely be explained by an increasing and ageing population
- A proportion do fail, many of these are linked to wear particle induced osteolysis

## NJR 2012

National Joint Registry

www.njr.org.uk

Annual Report 2012

Surgical data to 31st December 2011

2012

84,643 knee joint replacement procedures in 2011

Average patient age 68

56% female

98% osteoarthritis

5,137 revisions

6.1% revision burden

84,643 knee joint replacement procedures in 2011

Average patient age 68

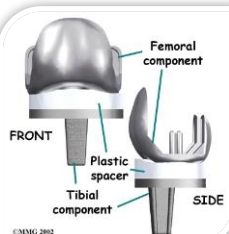
56% female

98% osteoarthritis

5,137 revisions

6.1% revision burden

## Total Knee Replacement (TKR) and Unicondylar



NJR 2012 – 91% TKR,  
1% patello-femoral replacement,  
8% unicondylar



93% fixed, 7% mobile

30% fixed, 70% mobile

Figure 2.17

Type of primary knee replacement procedures undertaken between 2005 and 2011.

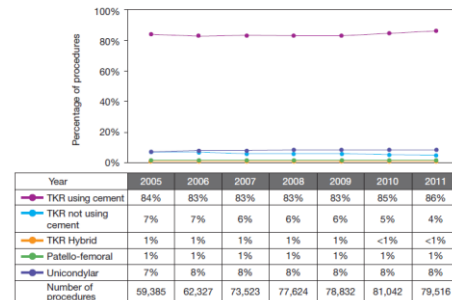
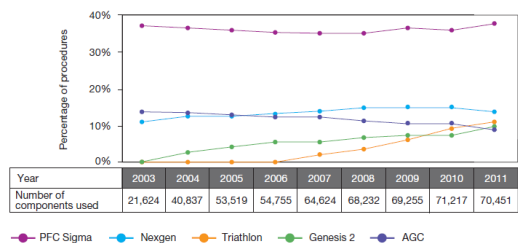


Figure 2.24

Top five total condylar knee brands, trends 2003 to 2011.



## NJR 2012

Figure 3.6

Risk of revision following primary knee replacement (cumulative hazard with 95% confidence intervals), by prosthesis type.

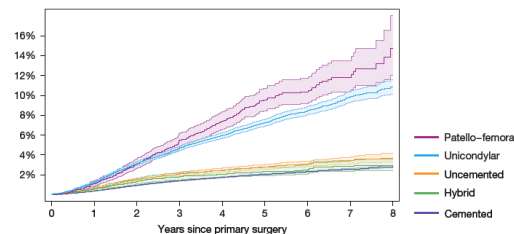


Table 3.17 Estimated medium-term revision rates after primary knee replacement by fixation, constraint and bearing type (95% confidence intervals).

	Year 4	Year 5	Year 6	Year 7	Year 8
All cemented	1.74%	2.04%	2.30%	2.55%	2.82%
Cemented, unconstrained, fixed	(1.62-1.79)	(1.92-2.10)	(2.24-2.39)	(2.47-2.64)	(2.71-2.86)
Cemented, unconstrained, mobile	1.58%	1.84%	2.10%	2.34%	2.62%
Cemented, posterior-stabilised, fixed	(1.52-1.64)	(1.77-1.91)	(2.02-2.19)	(2.24-2.44)	(2.48-2.77)
Cemented, posterior-stabilised, mobile	2.25%	2.56%	2.72%	2.92%	3.13%
Uncemented	2.03%	2.25%	2.52%	2.79%	3.09%
Uncemented, hybrid, unconstrained, fixed	(1.77-1.98)	(2.12-2.38)	(2.39-2.67)	(2.62-2.98)	(2.86-3.26)
Uncemented, hybrid, unconstrained, mobile	2.60%	2.94%	3.43%	3.63%	3.63%
All uncemented	(2.19-3.03)	(2.48-3.53)	(2.86-4.11)	(2.96-4.46)	(2.96-4.46)
All hybrid	2.42%	2.73%	3.10%	3.44%	3.67%
All hybrid, unconstrained, fixed	(2.24-2.67)	(2.55-3.04)	(2.82-3.38)	(3.11-3.81)	(3.29-4.14)
All hybrid, unconstrained, mobile	2.03%	2.39%	2.49%	2.84%	2.96%
All unicondylar	(1.69-2.48)	(1.93-2.75)	(2.08-2.98)	(2.36-3.43)	(2.43-3.68)
Unicondylar, fixed	6.09%	7.23%	8.39%	9.38%	10.14%
Unicondylar, mobile	(5.52-6.73)	(6.55-7.98)	(7.57-9.31)	(8.35-10.54)	(9.84-11.83)
All patello-femoral	5.66%	5.51%	5.03%	4.51%	4.07%
Other/unknown	(5.57-5.94)	(4.49-10.71)	(0.17-11.70)	(10.33-19.51)	(12.01-18.00)
All types	3.70%	4.24%	4.72%	5.42%	6.02%
	(3.09-4.44)	(3.65-4.93)	(3.93-5.69)	(4.65-6.59)	(4.81-7.53)
	2.23%	2.64%	2.99%	3.36%	3.71%
	(2.18-2.29)	(2.58-2.70)	(2.92-3.07)	(3.27-3.45)	(3.58-3.84)


## Indications for knee revision surgery (NJR 2012 p103)

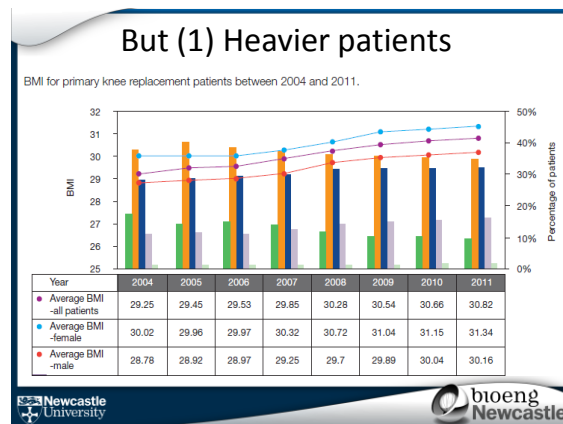
Aseptic loosening	35%
Pain	16%
Lysis	10%
Wear of PE component	10%
Instability	14%
Infection	23%
Malalignment	7%
Stiffness	5%
Progressive arthritis remaining	8%
Others	17%


## Australian Joint Registry 2012

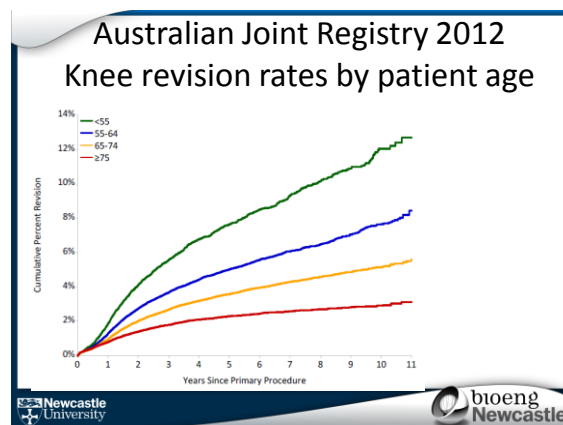
Table KT6: Primary Total Knee Replacement by Reason for Revision


Reason for Revision	Number	Percent
Loosening/Lysis	2960	30.0
Infection	2145	21.7
Patellofemoral Pain	1339	13.6
Pain	886	9.0
Instability	577	5.8
Arthrofibrosis	376	3.8
Fracture	234	2.4
Malalignment	213	2.2
Patella Erosion	199	2.0
Incorrect Sizing	148	1.5
Wear Tibial Insert	140	1.4
Metal Sensitivity	130	1.3
Other	533	5.4
<b>TOTAL</b>	<b>9880</b>	<b>100.0</b>


Newcastle University 



- ## But (2) Younger patients
- There has been a dramatic increase in the number of knees implanted in the 45-64 age group from 2000 to 2008
  - Likely subject to more wear
  - “the greater risk of implant failure in younger patients, coupled with longer remaining life expectancy in this age group, will combine to produce even higher rates of revision” (Losina 2012)
- Newcastle University 



- ## Why *ex vivo* analysis of knee implants?
- There are no standard techniques to quantify *in vivo* wear rates and track the clinical performance of UHMWPE components in knee replacements
  - The most effective way to evaluate the *in vivo* performance of UHMWPE continues to be the analysis of retrieved components from revision surgery or autopsy
- Newcastle University 

- ## How to undertake *ex-vivo* analysis of knee implants?
- Semi-quantitative Hood analysis of UHMWPE articulating and non-articulating surfaces
  - Roughness and surface topography of femoral (metal) articulating surfaces
  - Roughness and surface topography of articulating and backside of tibial UHMWPE insert
  - Roughness and surface topography of (metal) tibial tray
- Newcastle University 

### Mitutoyo Quick Scope vision measuring microscope



### Ex-Vivo Analysis UHMWPE



Selection of six retrieved Total Knee Replacement PE components with varying levels of macroscopic surface damage



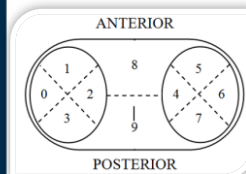
### Hood<sup>1</sup> Analysis: Surface Damage Modes

1. **Surface Deformation** - Areas where there is evidence of permanent deformation occurring on or around the articulating surface
2. **Pitting** - Depressions in the articulating surface
3. **Embedded Debris** - Recognised by a colour and/or texture difference
4. **Scratching** - Indented lines generally found in an anterior-posterior direction and the areas of wear
5. **Burnishing** - Areas that have become highly polished
6. **Abrasion** - Areas in which the UHMWPE has a shredded or tufted appearance
7. **Delamination** - Areas in which a large sheet of UHMWPE has been removed with evidence around the periphery of a subsurface failure mechanism occurring parallel to the articulating surface

1. Hood et al (JBoneMinRes)1993 Retrieval analysis of total knee prostheses: A method and its application to 48 total condyle prostheses



### Hood Analysis



- Tibial UHMWPE articulating surface divided into 10 sections
- In each section a score 0, 1, 2 or 3 is given for each surface damage mode
  - 0 = Damage mode not observed
  - 1 = Damage mode observed on <10%
  - 2 = Damage mode observed 10-50%
  - 3 = Damage mode observed >50%
- Total degradation score = sum of all surface damage mode scores for all 10 sections
- Maximum degradation score = 210 (i.e. 3 x 10 x 7 = 210)



### Hood Analysis

KXXX Hood Analysis										
Assessor:	A Other									
Date:	xx/xx/xx									
	0	1	2	3	4	5	6	7	8	9
Surface Deformation										
Pitting										
Embedded Debris										
Scratching										
Burnishing										
Abrasion										
Delamination										
										<b>TOTAL</b>



### Hood Analysis Limitations

- Inter- and Intra- Observer variability
- Semi-quantitative
- Grade bands too broad?
- Total score gives no indication of location of wear



## Backside wear

- Important as smaller, more reactive PE particles produced here (Conditt et al, 2005)
- Rao et al 2002, 6 sections + each of the 7 Hood damage modes, graded 0-3
- Conditt et al 2005, 4 sections

Newcastle University

## Backside wear

- Wasielewski et al (2004)
- Identification patterns for backside wear
- Same 7 damage modes are used as in the Hood analysis

Newcastle University

## Ex-vivo analysis: surface topography

- Roughness and surface topography measurements are taken using a Zygo NewView 5000 non-contacting 3D profilometer
- Vertical resolution of better than one nanometre
- Measurements include
  - $S_q$  – Root Mean Squared Roughness
  - $S_a$  – Average Roughness
  - $S_{sk}$  – Roughness Skew

Newcastle University

## Surface topography – femoral

Lateral Medial

(a) Unworn  $S_q$ : 0.034  $\mu\text{m}$

(b) Worn  $S_q$ : 0.324  $\mu\text{m}$

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## Ex-Vivo Analysis Surface Topography - UHMWPE

(a) (b)

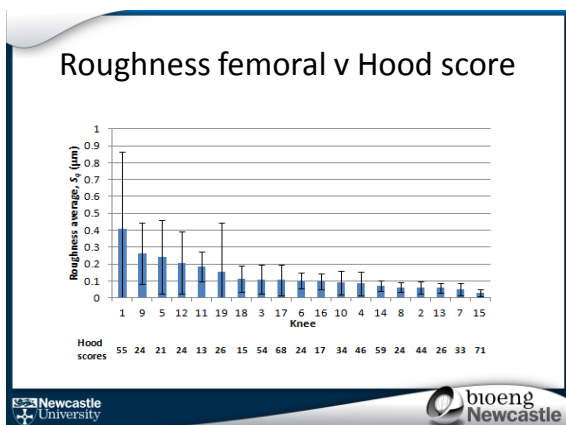
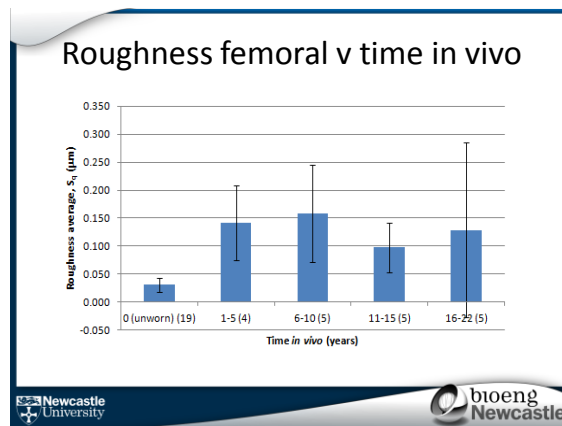
Surface topography of a UHMWPE Tibial component (a) unworn area ( $S_q$ : 0.311  $\mu\text{m}$ ) and (b) worn area ( $S_q$ : 1.467  $\mu\text{m}$ )

Newcastle University

## PILOT STUDY RESULTS (THANKS TO FREEMAN HOSPITAL FOR SUPPLY OF EXPLANTS)

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Knee	Age at Revision	BMI	Sex	Right or Left	Time in vivo (years)	Commented (C) or uncommented (U)	Knee Type	Indication for revision
1	81	27.5	M	R	20	U	Stryker Kinematic	Aseptic loosening
2	72	29.5	M	R	19	C	Smith and Nephew Genesis	Wear of UHMWPE, periprosthetic fracture
3	72	21.5	M	R	12	C	Stryker Kinemax	Infection
4	72	29.5	F	R	7	C	Plus Orthopaedics TC Plus	Wear of UHMWPE
5	56	28.5	M	R	7	C	Stryker Kinemax	Loosening
6	90	27	F	L	7	C	Biomet Maxin	Instability
7	55	26	M	R	22	C	Stryker Kinemax Plus	Infection
8	80	24	F	L	1	C	Biomet AGC V2 HPS	Instability, aseptic loosening, periprosthetic fracture
9	73	41.7	M	L	6	C	Biomet Dual Articular 2000	Infection
10	73	30	F	L	13	C	Stryker Kinemax	Wear of UHMWPE
11	77	25	M	R	2	C	DuPuy Nexlex S-ROM rotating hinge	Infection
12	79	31.5	M	R	5	C	DuPuy PFC Sigma	Infection
13	85	NK	F	R	20	C	Biomet AGC V2 HPS	Tibial loosening
14	82	25	M	L	19	C	Stryker Kinematic	Aseptic loosening and wear
15	79	32.7	M	L	14	C	Stryker Kinemax	Aseptic loosening
16	79	NK	F	R	7	C	DuPuy PFC Sigma	Infection
17	67	32	F	L	13	C	Stryker Kinemax	Wear of UHMWPE
18	67	38	M	R	3	C	DuPuy PFC Sigma	Fixed flexion, tight anterior compartment
19	49	33	F	L	14	U	Exacchib Ojestrak	Tibial loosening



- ### Summary of pilot study results
- All femoral components were shown to be up to 11x rougher
  - Mostly, this roughness was more apparent on the lateral condyle than the medial
  - Increase in roughness occurred relatively soon after implantation

**Northern Orthopaedic Research Sciences**

Dr. Thomas Joyce OBE FRACS  
Head of Technology  
Newcastle University

Dr. Susan C. Scholes  
Research Associate  
Newcastle University

Summary report for explanted knee prosthesis

**Basic Information**

Biomechanical reference: 0000  
 Date of explant: 10/02/2013  
 Primary diagnosis: Not available (NA)  
 Secondary diagnosis: NA  
 Time in vivo: 22 years

**Patient Information**

Female identification: Not known  
 Patient age at primary surgery: 61  
 Gender: Female  
 BMI: NA  
 Side: NA  
 Left/Right knee: NA  
 Patient physician (last name): NA  
 Patient knee score: NA  
 Knee Society Score (Knee score): NA (2002)

**Implant Information**

Left knee: Revision  
 Right knee: Revision  
 Left revision: NA  
 Right revision: NA  
 Type and model: Kinematic (Stryker Kinematic)  
 Primary diagnosis: NA  
 Secondary diagnosis: NA  
 Component/revision type: Kinematic

**Surface roughness measurements**

Parameters:  $S_d$  and  $S_q$  are the average roughness (Rz) and surface area (Da) values taken from the entire area being analysed.  $S_q$  is the average roughness.


Parameter	Mean	Width
Female component	0.02	0.18 - 0.31 - 0.52
Male component	0.02	0.07 - 0.21 - 0.32

Surface evaluation (based on mean of all RRS)  
 Average score (SD/RRR): 77 (small positive score = 2.0)

**Results**

Indication for revision suggest: Aseptic loosening (revision noted)  
 Implantation reason for failure: Surface alterations suggest aseptic loosening due to wear particles released extrinsically, along with fatigue failure related to distribution wear

• We continue to look at knee explants


*Topographical analysis of the femoral components of ex vivo total knee replacements*

**Susan C. Scholes, Emma Kennard, Rajkumar Gangadharan, David Weir, Jim Holland, David Deehan & Thomas J. Joyce**

**Journal of Materials Science: Materials in Medicine**  
 Official Journal of the European Society for Biomaterials

ISSN 0957-4530  
 Volume 24  
 Number 2

Figure 1: In vivo wear (average) bearing pre-revision surgery (NA to NA)

J Mater Sci: Mater Med (2013) 24:547-554  
 DOI 10.1007/s10856-012-4815-z

• Examination of failed TKR

**n.s.t.c.**  
 Newcastle Surgical Training Centre

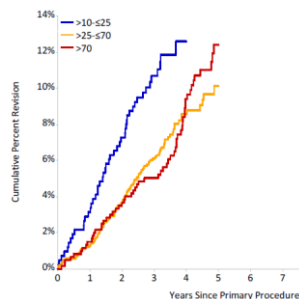
Freeman Hospital,  
 Newcastle upon Tyne

## DePuy LCS® Duofix™ knee

- Global revision rate 0.57%, higher in Australia, 1.34% revision rate (2009)
- DePuy recalled
- Willis-Owen, JBJS 2011, 8% revision rate
- “A complete explanation of the cause of this problem has not been made available by the manufacturer”
- Why not?



## Australian Joint Registry 2012



- LCS Duofix knee
- By surgeon number of procedures/year
- >10-25: 10.7% revision rate at 3 yrs
- 26-70: 10.1% revision rate at 5 years
- >70: 12.4% revision rate at 5 years
- “2,614 procedures”

## Overview

- Tribology
- Why undertake ex vivo analysis
- Hip prostheses
- Knee prostheses

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